

Appln. No.: 10/688,095

Attorney Docket No. 10541-1865

I. Amendments to the Claims

1. (Cancelled)

2. (Cancelled)

3. (Cancelled)

4. (Currently Amended) ~~The system according to claim 1,~~ A system for controlling an active suspension of a vehicle, having a bounce transmissibility, a roll transmissibility, and a pitch transmissibility, where the bounce, pitch, and roll transmissibilities vary with respect to a frequency of vibration acting upon the vehicle, the system comprising:

a tunable device configured for adjusting stiffness and damping of the active suspension; and

a controller in communication with the tunable device, the controller being configured to sense the frequencies of vibration and provide a control signal to the tunable device, wherein the control signal is based on a bounce component, a roll component, and a pitch component dependent on the bounce, pitch, and roll transmissibility at the sensed frequency wherein the control signal includes a ride control component, a handling control component, and a dive/squat control component.



BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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5. (Original) The system according to claim 4, wherein the control signal is based on the relationship

$$\begin{aligned} \text{ControlSignal} = & \beta_1 \times \text{TotalRideControl} \\ & + \beta_2 \times \text{HandlingControl} \\ & + \beta_3 \times \text{DiveSquatControl} \end{aligned}$$

where β_i are coefficients calculated based on the frequency of vibration and a summation of β_i is 1.

6. (Original) The system according to claim 4, wherein the ride control component includes a bounce control component, a roll control component, and a pitch control component.

7. (Original) The system according to claim 6, wherein the ride control is based on the relationship

$$\begin{aligned} \text{RideControl} = & \alpha_1 \times \text{BounceRideControl} \\ & + \alpha_2 \times \text{PitchRideControl} \\ & + \alpha_3 \times \text{RollRideControl} \end{aligned}$$

where α_i are coefficients calculated based on the frequency of vibration and a summation of α_i is 1.



BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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8. (Currently Amended) The system according to claim 4, wherein the controller includes a plurality of control strategies corresponding to a plurality of frequency ranges, and the control signal is based on a control strategy of the plurality of control strategies corresponding to a frequency range of the plurality of frequency ranges that includes the frequency of vibration.

9. (Original) The system according to claim 8, wherein the plurality of frequency ranges includes a low frequency range, a body mode frequency range, a medium frequency range, a wheel hop frequency range, and a high frequency range.

10. (Original) The system according to claim 8, wherein the plurality of control strategies includes a passive suspension control strategy, a small stiffness and skyhook control strategy, a low damping control strategy, a high damping control strategy and stiff suspension strategy.

11. (Original) The system according to claim 10, wherein the bounce control component is based on the relationship

$$\begin{aligned} \text{BounceControlComponent} = & \frac{A_1}{\varepsilon + \sum_{i=1}^s A_i} \times \text{PassiveSuspension} \\ & + \frac{A_2}{\varepsilon + \sum_{i=1}^s A_i} \times \text{Soft_StiffnessControl} + \frac{A_2}{\varepsilon + \sum_{i=1}^s A_i} \times \text{SkyhookControl} \end{aligned}$$

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HOFFER
GILSON
& LIONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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$$\begin{aligned}
& + \frac{A_3}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping} \\
& + \frac{A_4}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{HighDamping} \\
& + \frac{A_5}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping}
\end{aligned}$$

where A_i are estimated amplitudes of the bounce acceleration for the corresponding frequency ranges, wherein A_1 corresponds to the low frequency range, A_2 corresponds to the body mode frequency range, A_3 corresponds to the medium frequency range, A_4 corresponds to the wheel hop frequency range, and A_5 corresponds to the high frequency range, and ε is a small number selected to avoid singularity.

12. (Original) The system according to claim 8, wherein the pitch control component is based on the relationship

$$\begin{aligned}
\text{PitchControlComponent} = & \frac{A_1}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{PassiveSuspension} \\
& + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{Soft_StiffnessControl} + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{SkyhookControl} \\
& + \frac{A_3}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping}
\end{aligned}$$



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PO Box 10395
Chicago, IL 60611-5599

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$$+ \frac{A_4}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{HighDamping}$$

$$+ \frac{A_5}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping}$$

where A_i are estimated amplitudes of the pitch acceleration for the corresponding frequency ranges, wherein A_1 corresponds to the low frequency range, A_2 corresponds to the body mode frequency range, A_3 corresponds to the medium frequency range, A_4 corresponds to the wheel hop frequency range, and A_5 corresponds to the high frequency range, and ε is a small number selected to avoid singularity.

13. (Original) The system according to claim 8, wherein the roll control component is based on the relationship

$$\begin{aligned} \text{RollControlComponent} = & \frac{A_1}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{PassiveSuspension} \\ & + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{Soft_StiffnessControl} + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{SkyhookControl} \\ & + \frac{A_3}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping} \\ & + \frac{A_4}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{HighDamping} \end{aligned}$$

BRINKS
HOFFER
GILSON
& LIONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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$$+ \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times LowDamping$$

where A_i are estimated amplitudes of the roll acceleration for the corresponding frequency ranges, wherein A_1 corresponds to the low frequency range, A_2 corresponds to the body mode frequency range, A_3 corresponds to the medium frequency range, A_4 corresponds to the wheel hop frequency range, and A_5 corresponds to the high frequency range, and ε is a small number selected to avoid singularity.

14. (New) A system for controlling an active suspension of a vehicle, having a bounce transmissibility, a roll transmissibility, and a pitch transmissibility, where the bounce, pitch, and roll transmissibilities vary with respect to a frequency of vibration acting upon the vehicle, the system comprising:

a tunable device configured for adjusting stiffness and damping of the active suspension wherein the tunable device is a compressible fluid strut; and

a controller in communication with the tunable device, the controller being configured to sense the frequencies of vibration and provide a control signal to the tunable device, wherein the control signal is based on a bounce component, a roll component, and a pitch component dependent on the bounce, pitch, and roll transmissibility at the sensed frequency.

BRINKS
HOFFER
GILSON
& LIONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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15. (New) A system for controlling an active suspension of a vehicle, having a bounce transmissibility, a roll transmissibility, and a pitch transmissibility, where the bounce, pitch, and roll transmissibilities vary with respect to a frequency of vibration acting upon the vehicle, the system comprising:

a tunable device configured for adjusting stiffness and damping of the active suspension;

a controller in communication with the tunable device, the controller being configured to sense the frequencies of vibration and provide a control signal to the tunable device, wherein the control signal is based on a bounce component, a roll component, and a pitch component dependent on the bounce, pitch, and roll transmissibility at the sensed frequency wherein the controller includes a plurality of control strategies corresponding to a plurality of frequency ranges, and the control signal is based on a control strategy of the plurality of control strategies corresponding to a frequency range of the plurality of frequency ranges that includes the frequency of vibration; and

wherein the plurality of frequency ranges includes a low frequency range, a body mode frequency range, a medium frequency range, a wheel hop frequency range, and a high frequency range.

16. (New) The system according to claim 15, wherein the plurality of control strategies includes a passive suspension control strategy, a

BRINKS
HOFFER
GILSON
& LIONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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small stiffness and skyhook control strategy, a low damping control strategy, a high damping control strategy and stiff suspension strategy.

17. (New) The system according to claim 15, wherein the bounce control component is based on the relationship

$$\begin{aligned}
 \text{BounceControlComponent} = & \frac{A_1}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{PassiveSuspension} \\
 & + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{Soft_StiffnessControl} + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{SkyhookControl} \\
 & + \frac{A_3}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping} \\
 & + \frac{A_4}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{HighDamping} \\
 & + \frac{A_5}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping}
 \end{aligned}$$

where A_i are estimated amplitudes of the bounce acceleration for the corresponding frequency ranges, wherein A_1 corresponds to the low frequency range, A_2 corresponds to the body mode frequency range, A_3 corresponds to the medium frequency range, A_4 corresponds to the wheel hop frequency range, and A_5 corresponds to the high frequency range, and ε is a small number selected to avoid singularity.

BRINKS
HOFER
GILSON
LIONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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18. (New) The system according to claim 15, wherein the pitch control component is based on the relationship

$$\begin{aligned}
 \text{PitchControlComponent} = & \frac{A_1}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{PassiveSuspension} \\
 & + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{Soft_StiffnessControl} + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{SkyhookControl} \\
 & + \frac{A_3}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping} \\
 & + \frac{A_4}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{HighDamping} \\
 & + \frac{A_5}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping}
 \end{aligned}$$

where A_i are estimated amplitudes of the pitch acceleration for the corresponding frequency ranges, wherein A_1 corresponds to the low frequency range, A_2 corresponds to the body mode frequency range, A_3 corresponds to the medium frequency range, A_4 corresponds to the wheel hop frequency range, and A_5 corresponds to the high frequency range, and ε is a small number selected to avoid singularity.

BRINKS
HOFFER
GILSON
ALONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599

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19. (New) The system according to claim 15, wherein the roll control component is based on the relationship

$$\begin{aligned}
 \text{RollControlComponent} = & \frac{A_1}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{PassiveSuspension} \\
 & + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{Soft_StiffnessControl} + \frac{A_2}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{SkyhookControl} \\
 & + \frac{A_3}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping} \\
 & + \frac{A_4}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{HighDamping} \\
 & + \frac{A_5}{\varepsilon + \sum_{i=1}^5 A_i} \times \text{LowDamping}
 \end{aligned}$$

where A_i are estimated amplitudes of the roll acceleration for the corresponding frequency ranges, wherein A_1 corresponds to the low frequency range, A_2 corresponds to the body mode frequency range, A_3 corresponds to the medium frequency range, A_4 corresponds to the wheel hop frequency range, and A_5 corresponds to the high frequency range, and ε is a small number selected to avoid singularity.

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& LIONE

BRINKS HOFER GILSON & LIONE
PO Box 10395
Chicago, IL 60611-5599